

## BIR O'LCHOVLI HOLATDA MODDANING KO'CHISH TENGLAMASI VA UNI YECHIMI

*T.O.Dzhiyanov, M.H.Turayev.*

Samarkand State University, Samarkand, Uzbekistan

Bir o'lchovli holatda moddaning ko'chish tenglamalari quydagi ko'rinishda yoziladi [8].

$$\rho \frac{\partial S_{al}}{\partial t} + \rho \frac{\partial S_{sl}}{\partial t} + \theta_l \frac{\partial C_l}{\partial t} = \theta_l D_l \frac{\partial^2 C_l}{\partial x^2} - \theta_l v_l \frac{\partial C_l}{\partial x} + \alpha(C_m - C_l), \quad (3.1.1)$$

$$(l = 1; 2; m = 3 - l),$$

Bu yerda  $t$  – vaqt,  $s$ ,  $x$  – masofa,  $m$ ,  $D_l$  – bo'ylama dispersiyasi koeffitsienti,  $m^2/s$ ,  $v_l$  – suyuqlik tezligi,  $m/s$ ,  $v_1 < v_2$ ,  $C_l$  – suyuqlikdagi moddaning miqdori,  $S_{al}$  va  $S_{sl}$  – kechiktirilgan moddaning konsentratsiyasi,  $m^3/kg$ ,  $\theta_l$  – sohaning g'ovakligi,  $m^3/m^3$ ,  $\rho$  – muhit zichligi,  $kg/m^3$ ,  $\alpha$  – sohalar orasidagi massa almashinuvi koeffitsienti,  $s^{-1}$ .

Har bir soha bo'limida moddalarning cho'kishi kinetik tenglamalarga muvofiq qaytarilish tarzda sodir bo'ladi.

$$\rho \frac{\partial S_{al}}{\partial t} = \theta_l k_{al} C_l - \rho k_{adl} S_{al}, \quad (l = 1, 2), \quad (3.1.2)$$

$$\rho \frac{\partial S_{sl}}{\partial t} = \theta_l k_{sl} C_l - \rho k_{sdl} S_{sl}, \quad (l = 1, 2), \quad (3.1.3)$$

Bu yerda  $k_{al}$ ,  $k_{sl}$  – suyuqlik fazadan  $l$  qattiq fazaga moddaning cho'kish koeffitsientlari,  $s^{-1}$ ,  $k_{adl}$ ,  $k_{sdl}$  – moddaning qattiq fazadan ajralib chiqish va suyuqlikka o'tish koeffitsientlari,  $s^{-1}$ .

Dastlab sof (moddasiz) suyuqlik bilan to'yingan muhitga vaqtning dastlabki paytidan boshlab suyuqlik  $c_0$  moddasining doimiy konsentratsiyasi bilan to'yingan bo'lsin. Keling, konsentratsiya maydoni muhitning o'ng chegarasiga yetib bormaydigan

$x = \infty$  vaqt davrlarini ko'rib chiqaylik. Belgilangan ma'lumotlarga ko'ra, masalaning boshlang'ich va chegaraviy shartlari quyidagi ko'rinishga ega

$$C_i(0, x) = 0, S_{al}(0, x) = 0, S_{sl}(0, x) = 0, \quad (3.1.4)$$

$$C_i(t, 0) = c_0, \quad (3.1.5)$$

$$\frac{\partial C_l}{\partial x}(t, \infty) = 0, \quad l = 1, 2. \quad (3.1.6)$$

**Sonli yechim va natijalar.** (3.1.1) - (3.1.6) masala chiziqli bo'lsada, analitik yechimni olish qiyin, chunki sohalarning har birida bir vaqtning o'zida uchta maydonni topish kerak. Shuning uchun masalani yechish uchun [9] chekli ayirmalar usulidan foydalanamiz. Ko'rib chiqilayotgan  $\Omega = \{(t, x), 0 \leq t \leq T, 0 \leq x \leq \infty\}$  maydonda yo'nalishlar bo'yicha yagona to'r joriy etiladi

$$\bar{\omega}_{\tau h} = \left\{ (t_j, x_i); t_j = \tau j, x_i = ih, \tau = \frac{T}{J}, i = \overline{0, I}, j = \overline{0, J} \right\}$$

Bu yerda  $I = [0, x_I], x_I = ih$  segmenti bo'lishi uchun yetarlicha katta butun son tanlangan,  $C_i, S_{ai}$  va  $S_{si}$  maydonlarida hisoblangan o'zgarishlar maydonini bir-biriga moslashtiriladi,  $h = x$  yo'nalishidagi to'r qadami.

Oshkor to'r sohasida

$$\omega_{\tau h} = \left\{ (t_j, x_i); t_j = \tau j, x_i = ih, \tau = \frac{T}{J}, j = \overline{1, J}, i = \overline{1, I-1} \right\}$$

(1), (2), (3) tenglamalar quyidagicha approksimatsiya qilinadi

$$\begin{aligned} & \rho \frac{(S_{al})_i^{j+1} - (S_{al})_i^j}{\tau} + \rho \frac{(S_{sl})_i^{j+1} - (S_{sl})_i^j}{\tau} + \theta_l \frac{(C_l)_i^{j+1} - (C_l)_i^j}{\tau} = \\ & = \theta_l D_l \frac{(C_l)_{i-1}^{j+1} - 2(C_l)_i^{j+1} + (C_l)_{i+1}^{j+1}}{h^2} - \theta_l \nu_l \frac{(C_l)_i^{j+1} - (C_l)_{i-1}^{j+1}}{h} + \alpha (C_m)_i^j - \alpha (C_l)_i^j, \end{aligned} \quad (3.1.7)$$

( $l = 1, 2; m = 2, 1$ ),

$$\rho \frac{(S_{al})_i^{j+1} - (S_{al})_i^j}{\tau} = \theta_l k_{al} (C_l)_i^j - \rho k_{adl} (S_{al})_i^{j+1}, \quad (l = 1, 2), \quad (3.1.8)$$

$$\rho \frac{(S_{sl})_i^{j+1} - (S_{sl})_i^j}{\tau} = \theta_l k_{sl} (C_l)_i^j - \rho k_{sdl} (S_{sl})_i^{j+1}, \quad (l=1,2), \quad (3.1.9)$$

Bu yerda  $(C_l)_i^j$ ,  $(S_{al})_i^j$ ,  $(S_{sl})_i^j - C_l(t, x)$ ,  $S_{al}(t, x)$ ,  $S_{sl}(t, x)$ ,  $(l=1,2)$  funksiyalarning  $(t_j, x_i)$  nuqtadagi to'r qiymatlari.

Aniq to'r (3.1.8), (3.1.9) tenglamalaridan,  $(S_{al})_i^{j+1}$ ,  $(S_{sl})_i^{j+1}$  ni aniqlaymiz

$$(S_{al})_i^{j+1} = p_{1l} (S_{al})_i^j + p_{2l}, \quad (l=1; 2), \quad (3.1.10)$$

$$(S_{sl})_i^{j+1} = q_{1l} (S_{sl})_i^j + q_{2l}, \quad (l=1; 2), \quad (3.1.11)$$

Bu yerda

$$p_{1l} = \frac{1}{1 + \tau k_{adl}}, \quad p_{2l} = \frac{\tau \theta_l k_{al}}{\rho + \rho \tau k_{adl}} (C_l)_i^j, \quad (l=1; 2),$$

$$q_{1l} = \frac{1}{1 + \tau k_{sdl}}, \quad q_{2l} = \frac{\tau \theta_l k_{sl}}{\rho + \rho \tau k_{sdl}} (C_l)_i^j, \quad (l=1; 2).$$

To'r tenglamalari (3.1.7) ko'rinishga keltiriladi

$$A_l (C_l)_{i-1}^{j+1} - B_l (C_l)_i^{j+1} + E_l (C_l)_{i+1}^{j+1} = -(F_l)_i^j, \quad (l=1,2), \quad (3.1.12)$$

Bu yerda

$$A_l = \frac{\theta_l D_l \tau}{h^2} + \frac{\theta_l \nu_l \tau}{h},$$

$$B_l = \theta_l + \frac{2\theta_l D_l \tau}{h^2} + \frac{\theta_l \nu_l \tau}{h},$$

$$E_l = \frac{\theta_l D_l \tau}{h^2},$$

$$(F_l)_i^j = (\theta_l - \alpha \tau) (C_l)_i^j + \alpha \tau (C_m)_i^j - \rho ((S_{al})_i^{j+1} - (S_{al})_i^j) - \rho ((S_{sl})_i^{j+1} - (S_{sl})_i^j),$$

$(l=1,2; m=2,1)$ .

Yechimlarni quyidagicha tartibda hisoblaymiz. (3.1.10), (3.1.11) ga ko'ra  $(S_{al})_i^{j+1}$ ,  $(S_{sl})_i^{j+1}$  aniqlanadi, so'ngra  $(C_l)_i^{j+1}$ ,  $(l=1,2)$  – (3.1.12) chiziqli tenglamalar tizimini progonka usuli bilan yechiladi. Chunki  $p_{1l}$ ,  $q_{1l} < 1$  sxemalar uchun (3.10), (3.1.11) barqaror va (3.1.12) uchun progonka usulining barqarorlik shartlari bajariladi.

Hisoblashda dastlabki parametrlarning quyidagi qiymatlaridan foydalanilgan:

$$v_1 = 10^{-4} \text{ m/s}, \quad v_2 = 10^{-5} \text{ m/s}, \quad D_1 = v_1 \cdot \alpha_l, \quad D_2 = v_2 \cdot \alpha_l, \quad \theta_1 = 0,1, \quad \theta_2 = 0,4$$
$$k_{a1} = 3 \cdot 10^{-4} \text{ s}^{-1}, \quad k_{ad1} = 2,5 \cdot 10^{-4} \text{ s}^{-1}, \quad k_{s1} = 4 \cdot 10^{-4} \text{ s}^{-1}, \quad k_{sd1} = 2 \cdot 10^{-4} \text{ s}^{-1}, \quad \rho = 1800 \text{ kg/m}^3,$$
$$k_{a2} = 4 \cdot 10^{-4} \text{ s}^{-1}, \quad k_{ad2} = 2 \cdot 10^{-4} \text{ s}^{-1}, \quad k_{s2} = 5 \cdot 10^{-4} \text{ s}^{-1}, \quad k_{sd2} = 10^{-4} \text{ s}^{-1}, \quad \alpha_l = 0,005 \text{ m}.$$

### **Foydalanilgan adabiyotlar ro'yxati**

1. Barenblatt G.I., Entov V.M. and Ryzhik V.M. Theory of Fluid Flow Through Natural Rocks. Kluwer Academic, Dordrecht, The Netherlands. 1990.
2. Van Golf-Racht T.D. Fundamentals of Fractured Reservoir Engineering. Developments in Petroleum Science, Vol. 12. Elsevier. 1982 y. 732 p.
3. Sahimi M. Flow and Transport in Porous Media and Fractured Rock. From Classical Methods to Modern Approaches. Second, Revised and Enlarged Edition. WILEY-VCH Verlag GmbH & Co. KGaA. 2011.
4. Leij F.L., Bradford S.A. Colloid transport in dual-permeability media // Journal of Contaminant Hydrology. 150.- 2013.-P. 65–76.
5. Khuzhayorov B. Kh, Djiyanov T.O. Solute Transport with nonequilibrium adsorption in an inhomogeneous porous medium // Scientific journal «problems of computational and applied mathematics». -2017. -№ 3(9). – P. 63-70.
6. Samarskiy A.A. The theory of difference scheme. M. The science. 1977. P. 656.
7. Bradford S.A., Simunek J., Bettahar M., van Genuchten M.T., Yates S.R. Modeling colloid attachment, straining, and exclusion in saturated porous media // Environmental Science & Technology. 37.-2003.- P. 2242–2250.

8. Bradford S.A., Torkzaban S. Colloid transport and retention in unsaturated porous media: A review of interface-, collector-, and pore-scale processes and models // *Vadose Zone Journal*. 7.- 2008.- P. 667–681.

9. Elimelech M. et al. Particle Deposition and Aggregation Measurement, Modelling, and Simulation. Butterworth-Heinemann.- Oxford, England, 1995. 10. Gitis V., Rubinstein I., Livshits M., Ziskind M. Deep-bed filtration model with multistage deposition kinetics // *Chemical Engineering Journal*. 163.- 2010.